

1 **DEVICE AND METHOD FOR ENHANCING**
2 **TRANSDERMAL FLUX OF AGENTS BEING DELIVERED**
3 **OR SAMPLED**

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5 **Cross-Reference to Related Applications**

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7 A claim is made, under 35 USC 119 (e), to the benefit of the filing of
8 US Patent Application Serial No. 60/019,990 filed June 18, 1996.

9
10 **Field of the Invention**

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12 The present invention relates to transdermal agent delivery and
13 sampling. More particularly, this invention relates to the transdermal delivery
14 of agents, such as peptides and proteins, as well as the transdermal
15 sampling of agents, such as glucose, body electrolytes and substances of
16 abuse, such as but not limited to alcohol and illicit drugs. The present
17 invention uses skin-piercing microblades to enhance the transdermal flux of
18 the agents during transdermal delivery or sampling and anchoring elements
19 to assist in retaining the delivery or sampling device in the skin.

20
21 **Background of the Invention**

22
23 Interest in the percutaneous or transdermal delivery of peptides and
24 proteins to the human body continues to grow with the increasing number of
25 medically useful peptides and proteins becoming available in large quantities
26 and pure form. The transdermal delivery of peptides and proteins still faces
27 significant problems. In many instances, the rate of delivery or flux of
28 polypeptides through the skin is insufficient to produce a desired therapeutic
29 effect due to the binding of the polypeptides to the skin. In addition,
30 polypeptides and proteins are easily degraded during and after penetration

1 into the skin, prior to reaching target cells. Likewise, the passive flux of water
2 soluble small molecules such as salts is limited.

3 One method of increasing the transdermal delivery of agents relies on
4 the application of an electric current across the body surface or on
5 "electrotransport". "Electrotransport" refers generally to the passage of a
6 beneficial agent, e.g., a drug or drug precursor, through a body surface such
7 as skin, mucous membranes, nails, and the like. The transport of the agent is
8 induced or enhanced by the application of an electrical potential, which
9 results in the application of electric current, which delivers or enhances
10 delivery of the agent. The electrotransport of agents through a body surface
11 may be attained in various manners. One widely used electrotransport
12 process, iontophoresis, involves the electrically induced transport of charged
13 ions. Electroosmosis, another type of electrotransport process, involves the
14 movement of a solvent with the agent through a membrane under the
15 influence of an electric field. Electroporation, still another type of
16 electrotransport, involves the passage of an agent through pores formed by
17 applying a high voltage electrical pulse to a membrane. In many instances,
18 more than one of these processes may be occurring simultaneously to
19 different extents. Electrotransport delivery generally increases agent delivery,
20 particularly large molecular weight species (e.g., polypeptides) delivery rates,
21 relative to passive or non-electrically assisted transdermal delivery.
22 However, further increases in transdermal delivery rates and reductions in
23 polypeptide degradation during transdermal delivery are highly desirable.

24 One method of increasing the agent transdermal delivery rate involves
25 pre-treating the skin with, or alternatively co-delivering with the beneficial
26 agent, a skin permeation enhancer. The term "permeation enhancer" is
27 broadly used herein to describe a substance which, when applied to a body
28 surface through which the agent is delivered, enhances its electrotransport
29 flux. The mechanism may involve a reduction of the electrical resistance of
30 the body surface to the passage of the agent therethrough, an increase in the

1 permeability of the body surface, the creation of hydrophilic pathways through
2 the body surface, and/or a reduction in the degradation of the agent (e.g.,
3 degradation by skin enzymes) during electrotransport.

4 There have been many attempts to enhance transdermal flux by
5 mechanically puncturing the skin prior to transdermal drug delivery. See for
6 example U. S. Patent Nos. 5,279,544 issued to Gross et al., 5,250,023 issued
7 to Lee et al., and 3,964,482 issued to Gerstel et al. These devices utilize
8 tubular or cylindrical structures generally, although Gerstel does disclose the
9 use of other shapes, to pierce the outer layer of the skin. Each of these
10 devices provide manufacturing challenges, limited mechanical attachment of
11 the structure to the skin, and/or undesirable irritation of the skin.

12 As has been discussed, a variety of chemicals and mechanical means
13 have been explored to enhance transdermal flux. However, there is still a
14 need to provide a device suitable for increasing transdermal flux which device
15 is low-cost and which can be manufactured reproducibly (i.e., without
16 significant variation from device to device) in high volume production and to
17 improve the attachment of the device to the skin.

18 Description of the Invention

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20
21 The present invention provides a reproducible, high volume
22 production, low-cost device suitable for increasing transdermal flux and
23 improving attachment to the skin with minimal to no skin irritation. The device
24 generally comprises a structure that attaches to the skin more effectively than
25 the prior art devices. The invention comprises a plurality of microblades for
26 piercing and anchoring to the skin. The blades typically have a length of less
27 than about 0.4 mm and a width and thickness which is even smaller. In spite
28 of their small size, the blades can be made with an extremely reproducible
29 size and shape so that the microslits formed by the blades puncturing the
30 skin also have a very reproducible size and depth. Because the blades have

1 a small thickness (i.e., small relative to the width and length of the blades),
2 the blades produce less tissue damage for a given cross-section than a skin
3 piercing microneedle having a circular cross-section. The device of the
4 present invention pierces the stratum corneum of a body surface to form
5 pathways through which a substance (e.g., a drug) can be introduced (i.e.,
6 delivery) or through which a substance (e.g., a body electrolyte) can be
7 withdrawn (i.e., sampling).

8 In one aspect of the invention, the device comprises a sheet having a
9 plurality of openings therethrough, a plurality of microblades integral
10 therewith and extending downward therefrom, and means for anchoring the
11 device to a body surface. In the many different aspects of the invention, the
12 device is anchored to the body surface in any of plurality of ways, including
13 but not limited to, having an extension such as a prong or barb extending
14 from at least some of the microblades, having an opening extending
15 perpendicular through at least some of the microblades, covering essentially
16 the entire surface area of the skin contacting surface of the device with
17 adhesive except for one side of the microblades, orienting at least some of
18 the plurality of microblades at an angle of 90° to the remainder of the plurality
19 of microblades, orienting at least some of the plurality of microblades at an
20 angle within a range of about 1° to about 89° with respect to the remainder of
21 the plurality of microblades, providing a plurality of second openings through
22 the sheet which make the device more shapeable with respect to the body
23 surface. The device of the present invention can be used in connection with
24 drug delivery, body analyte or drug sampling, or both. Delivery devices for
25 use with the present invention include, but are not limited to, electrotransport
26 devices, passive devices, osmotic devices and pressure-driven devices.
27 Sampling devices for use with the present invention include, but are not
28 limited to, "reverse" electrotransport devices as disclosed in Glikfeld et al.,
29 U.S. Patent No. 5,279,543, passive devices, osmotic devices and negative
30 pressure driven devices.

1 The present invention also provides a high yield, low-cost method for
2 producing, in extremely reproducible fashion, the device of the present
3 invention.

4
5 **Brief Description of the Drawings**

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7 Figure 1 is a perspective exploded view of one embodiment of an
8 electrotransport agent delivery system with a blade array device according to
9 one embodiment of the present invention;

10 Figure 2 is an enlarged perspective view of the skin proximal side of
11 the blade array device in accordance with one embodiment of the present
12 invention;

13 Figure 3 is a partial top plan view of a blade array pattern in
14 accordance with one embodiment of the present invention for forming blades
15 with anchoring elements;

16 Figure 4 is partial top plan view of yet another embodiment of the
17 blade array pattern of Figure 3;

18 Figure 5 is an enlarged view of a portion of the blades of the blade
19 array pattern of Figure 3;

20 Figure 6 is an enlarged view of a blade tip in accordance with one
21 embodiment of the present invention;

22 Figure 7 is an enlarged view of a blade tip in accordance with another
23 embodiment of the present invention;

24 Figure 8 is a diagrammatic representation of a method for producing
25 blades of the present invention from the blade array pattern of figure 3;

26 Figure 9 is an enlarged cross-sectional view of angled blades in
27 accordance with one embodiment of the present invention;

28 Figures 10, 11 and 12 are yet other embodiments of the blades with
29 anchoring elements of the present invention;

1 Figure 13 is a right side elevational view of another embodiment of a
2 blade with an anchoring element;

3 Figure 14 is an end view of the blade of figure 13;

4 Figures 15 and 16 are another embodiment of the blade and an
5 anchoring element;

6 Figure 17 is a right side elevational view of a blade with anchoring
7 elements in accordance with one embodiment of the present invention;

8 Figure 18 is a cross-sectional view taken along line 18-18 of figure 17;

9 Figure 19 is a right side elevational view of another embodiment of a
10 blade with an anchoring element;

11 Figure 20 is an enlarged partial top plan view of still another
12 embodiment of the blade array pattern;

13 Figure 21 is an enlarged partial top plan view of yet another
14 embodiment of the blade array pattern;

15 Figure 22 is a bottom plan view of the electrotransport agent delivery
16 system of figure 1;

17 Figure 23 is a right side elevational view of the electrotransport agent
18 delivery system of figure 1;

19 Figure 24 is a rear elevational view of the electrotransport agent
20 delivery system of figure 1;

21 Figure 25 is a cross-sectional view taken along line 25-25 of the
22 assembled electrotransport agent delivery system of figure 23;

23 Figure 26 is a diagrammatic cross-sectional view of a passive agent
24 delivery system in accordance with one embodiment of the present invention;

25 Figure 27 is a diagrammatic cross-sectional view of another
26 embodiment of a passive agent delivery system in accordance with the
27 present invention;

28 Figure 28 is a diagrammatic cross-sectional view of a sampling system
29 in accordance with one embodiment of the present invention; and

1 Figure 29 is a diagrammatic cross-sectional view of another
2 embodiment of the blades of the present invention.

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Modes for Carrying Out the Invention

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6 Turning now to the drawings in detail, one embodiment of the device 2
7 of the present invention is generally shown in Figure 1 for use with
8 electrotransport delivery device 10. Device 2 is used for the percutaneous
9 administration or sampling of an agent. The terms "substance", "agent" and
10 "drug" are used interchangeably herein and broadly include physiologically or
11 pharmacologically active substances for producing a localized or systemic
12 effect or effects in mammals including humans and primates, avians, valuable
13 domestic household, sport or farm animals, or for administering to laboratory
14 animals such as mice, rats, guinea pigs, and the like. These terms also
15 include substances such as glucose, electrolyte, alcohol, illicit drugs, etc. that
16 can be sampled through the skin. The major barrier properties of the skin,
17 such as resistance to drug penetration, reside with the stratum corneum. The
18 inner division of the epidermis generally comprises three layers commonly
19 identified as stratum granulosum, stratum Malpighi, and stratum
20 germinativum. Once a drug penetrates below the stratum corneum, there is
21 substantially less resistance to permeation through the underlying stratum
22 granulosum, stratum Malpighi, and stratum germinativum layers for
23 absorption and circulation of drug into the body. The device of the present
24 invention is used to form microslits in the stratum corneum and produce a
25 percolation area in the skin for improved transdermal delivery or sampling of
26 an agent.

27 Device 2 comprises a plurality of microblades 4 (i.e., a blade array)
28 extending downward from one surface of a sheet or plate 6 (see Figure 2 in
29 which device 2 is in an inverted position to show the microblades). The
30 microblades 4 penetrate the stratum corneum of the epidermis when pressure

1 is applied to the device to increase the administration of or sampling of a
2 substance through a body surface. The term "body surface" as used herein
3 refers generally to the skin, mucous membranes, and nails of an animal or
4 human, and to the outer surface of a plant.

5 Furthermore, the device 2 of the present invention improves the
6 attachment of the device to the skin so that the percolation areas and a
7 continuous pathway are preserved during movement of the body surface. In
8 the embodiment shown in Figure 2, projections in the form of barbs 50 on at
9 least one of the blades 4 assist in anchoring the device 2 and any
10 corresponding device or structure used in combination therewith to the skin.
11 Barbs 50 can be on any number of the blades from one blade to all blades.
12 Other embodiments which assist to anchor the device to the skin will be
13 discussed below.

14 The microblades 4 are generally formed from a single piece of material
15 and are sufficiently sharp and long for puncturing the stratum corneum of the
16 skin. In one embodiment, the microblades 4 and the sheet 6 are essentially
17 impermeable or are impermeable to the passage of an agent. The sheet 6 is
18 formed with an opening 8 between the microblades 4 for enhancing the
19 movement of an agent therethrough. In the case of therapeutic agent (e.g.,
20 drug) delivery, the drug is released from a drug-containing reservoir (not
21 shown in Figure 2) through microslits formed by the microblades 4 cutting
22 through the stratum corneum, migrating down the outer surfaces of the
23 microblades and through the stratum corneum to achieve local or systemic
24 therapy. In the case of agent (e.g., body analyte) sampling, the analyte (or
25 interstitial fluid containing the analyte) migrates from the body through the
26 microslits in the stratum corneum which are cut by the microblades 4. In one
27 embodiment, the opening 8 corresponds to the portion of the sheet 6
28 occupied by each of the microblades prior to the blades being transpositioned
29 into the downward depending position. The number of microblades 4 per
30 opening 8 can be any number, preferably however between 1 and about 30

1 blades per opening. Furthermore, the number of openings per device and
2 the number of blades per device are independent. The device may have only
3 one opening and one microblade. The agent can be administered at a
4 controlled rate of release from the reservoir through an agent release rate
5 controlling material (not shown) covering the openings 8.

6 As is best shown in Figure 2, the microblades 4 have a thickness
7 which is much smaller than the width of the blades near their base, i.e., near
8 the point where the blades are attached to the plate 6. This blade geometry
9 provides maximum drug percolation area with a minimum blade penetration
10 area, and hence less tissue damage. The drug percolation area is the skin
11 area in contact with the blades which provides for drug penetration in the
12 skin. The microblades are shaped with the largest possible surface area with
13 a minimal cross-sectional area so as to give the largest possible percolation
14 area. Thin microblades are better than round protrusions for this purpose
15 because for the same cross-section, a thin blade produces more percolation
16 area and less tissue damage than a round protrusion. This is a crucial
17 advantage over the prior art round elements such as needles and tubes.
18 Thin microblades also require less insertion force than round protrusions.
19 The width of each blade can be any of a range of widths. The widths can be
20 different from blade to blade in the array pattern. Likewise, the width can be
21 variable along the length of the blade, as will be described in more detail
22 below. The width of the blade at the intersection of the blade and the body
23 surface after the blade array has been inserted is preferably in the range of
24 about 25 μm to about 500 μm , more preferably about 50 μm to about 400 μm ,
25 more preferably 100 μm to about 300 μm .

26 In one embodiment, the microblades 4 (Figure 5) are also provided
27 with slanted (i.e., angled) leading edges 64 to further reduce the insertion
28 force required to press the blades into the skin tissue. The angle of the
29 leading edge is designated as α . The slanted leading edges produce a cut
30 through the skin tissue that is equal to the full width of the blade 4 while

1 reducing the amount of metal that is in the skin tissue. In other words, a flat
2 leading edge (i.e., α is 90°) produces a blade with a larger amount of blade
3 material in the skin tissue than is produced by a blade having a slanted
4 leading edge. The leading edges of each blade can all be the same angle or
5 can be at different angles as shown in Figure 5. The angle α of each leading
6 edge can be any angle between about 10° to 90° , preferably between about
7 10° to 60° , more preferably about 10° to 40° . The leading edge can also be
8 segmented into two sections at different angles. For example, the first
9 segment can have an angle α between about 10° to 40° and then transition to
10 a second segment having an angle between 20° to 60° . Alternatively, the
11 leading edge of each blade can be arcuate (i.e., curved) in shape, having, for
12 example, a convex or concave shape. In one embodiment, the leading edge
13 is a curved tip across the entire width of the blade.

14 The microblades 4 are formed using a photo-etching process which is
15 described in detail hereinafter. This process allows the microblades 4 to be
16 reproducibly formed on a very small (i.e., tens of microns) scale. This
17 process also allows the microblades 4 to be formed in shapes which help
18 anchor device 2 to the skin. In one embodiment, the microblades 4 are
19 provided with barbs 50 (Figures 2, 3 and 5) in some fashion so that the
20 device 2 and any corresponding device attached thereto stays attached to the
21 skin after being applied with pressure. The degree of attachment and the
22 number and size of the barbs is such as to retain the delivery or sampling
23 device during the normal activity of the wearer, but not cause pain upon
24 removal. As the microblades are pressed into the skin tissue for use, the
25 leading edge 64 of each microblade cuts through and pushes aside the skin
26 tissue. After the microblades have come to rest in the skin, the skin due to its
27 elastic nature at least partially comes back together around the edges of the
28 microblades, in this way the surface 66 on each microblade having a barb 50
29 engages skin tissue and anchors the device in the skin. If the blade is left in
30 the skin for an extended period of time (e.g., 24 hours), the skin tissue begins

1 to heal together in the area behind the surface 66 of the barb thus improving
2 the anchoring of the device. Only one barb per blade is shown in the figures
3 but it is within the scope of the present invention that each blade can have a
4 plurality of barbs extending therefrom. The microblades, in one embodiment,
5 have a cross-section that is wider in the area of the skin distal end of the
6 blade than in the area of the skin proximal end, thus providing additional
7 anchoring of the distal end in the skin. For example, the blades can have an
8 "arrowhead" shape. Furthermore, the barbs 50 shown in the figures are in
9 the same plane as the blade, however the barbs can be oriented outside of
10 that plane for example by a separate bending step or by using a shaped
11 punch and die to produce a curve in the blade and barb. Curving the tips of
12 the blade outside the plane of the blade generally provides better anchoring.
13 Insertion of such blades causes the barbs to curve in the curve direction but
14 retraction causes them to return to their prior position. The resulting curved
15 cross-section of the blade can be, but is not limited to, angular, semi-circular,
16 C-shaped, or banana-shaped to effect a larger cross-section of openings in
17 the skin.

18 The plurality of microblades 4 for puncturing the stratum corneum are
19 present on one face surface 48 of the device 2 in any predetermined
20 arrangement, for example, as a cluster of blades spaced in rows having any
21 desired number, or in any spaced apart relation of one blade to each other.
22 The device 2 of the embodiment shown in Figures 1 and 2 is produced by the
23 pattern shown in Figure 3. Each blade has a width and thickness that
24 facilitates penetration of the stratum corneum without bending. In the
25 embodiment of Figure 3, there are six blades 4 in each opening 8 in sheet 6.
26 Each opening 8 in this embodiment is 1 mm long and 300 μm wide.
27 Correspondingly, the width of each blade is between about 137.5 μm to about
28 175 μm and the length is about 250 μm . The required length of the blades is
29 subject to variation of the body surface being penetrated and corresponds to
30 the natural thickness of the stratum corneum, for one of the principle features

1 of the invention is that the blades are to penetrate the stratum corneum into
2 the epidermis. Usually, the blades will be about 25 μm to about 400 μm in
3 length, with the length for most applications being between about 50 μm to
4 about 200 μm .

5 The pattern for any of the blade array devices of the present invention
6 are produced with a photo-etching process. A thin sheet or plate 6 of metal
7 such as stainless steel or titanium is etched photo-lithographically with
8 patterns containing blade-like structures. In general, a thin laminate dry
9 resist or wet resist is applied on a sheet about 7 μm to about 100 μm thick,
10 preferably about 25 μm to about 50 μm thick. The resist is contact exposed
11 using a mask having the desired pattern and is subsequently developed.
12 These operations are conducted in much the same way that they are for the
13 manufacture of a printed circuit board. The sheet is then etched using acidic
14 solutions. After the pattern has been etched through the sheet, the sheet is
15 placed on a die 52 (shown schematically in figure 8) having a plurality of
16 openings 56 corresponding to the openings 8 in the sheet. A punch 54
17 having a plurality of protrusions 58 corresponding to the openings in the
18 sheet and die is initially located above the sheet and die. At the initial stage,
19 the blades 4 are in the same plane as the rest of the sheet 6. The
20 protrusions 58 on the punch 54 are then pressed into the openings 56, thus
21 bending the blades 4 downward to be at an angle (e.g., substantially
22 perpendicular) to the plane of the sheet. The finished structure provides
23 blades 4 with an adjacent opening 8 for the passage of a substance
24 therethrough when the device 2 is applied to the skin. Rectangular openings
25 8 are shown in the figures but the invention encompasses the use of any
26 shape openings including, but not limited to, square, triangular, circular and
27 elliptical.

28 The sheet 6 in some areas can have additional etched openings 80
29 (Figure 4) to alleviate the curl created during punching and/or to provide for
30 flexibility in the dense blade array patterns because in some embodiments

1 the sheet becomes very stiff after punching. The openings can be any of a
2 variety of shapes (e.g., rectangular, circular, elliptical, triangular, etc.) The
3 openings also allow the sheet to be more easily curved to match the
4 curvature of the body surface to which it is to be attached which improves
5 anchoring of the device. The present invention maximizes the openings
6 through the sheet but with a sufficient number of horizontal and vertical
7 continuous portions in the sheet to prevent the sheet from being too flexible
8 (i.e., flimsy). If the openings are made too long in any one dimension, the
9 sheet will bend (i.e., crinkle). In addition, it is also possible to treat the
10 devices after punching with heat or plastic deformation such that the radius of
11 curvature of the sheet becomes equal to or somewhat smaller than the
12 curvature of the body, where it is to be attached to enhance anchoring. The
13 concave surface can be shaped to match the convex pattern of the body.

14 The blades 4 can be patterned with resist on both sides 48,49 and
15 subsequently etched simultaneously from both sides (Figure 7) to achieve
16 maximum pattern resolution for a given sheet thickness and to produce a
17 knife-like edge that can not be achieved with conventional stamping and
18 punching processes. Alternatively, the blades 4 can be patterned and etched
19 from one side (i.e., side 49) only (Figure 6). When etching from one side
20 only, the etching process can be controlled to etch selective depths in the
21 plate 6 along the length of the blades (e.g., at the blade tips) to produce a
22 single angle 60 at the tip of the blade which maximizes the sharpness of the
23 knife-like edge of the blade. In this embodiment, the lithography process
24 produces a portion of the blade that is thinner than the remainder of the
25 thickness of the blade and of the sheet. The lithography process also can
26 produce very small dimensioned elements for the anchoring and the
27 penetration aspects of the invention.

28 In another embodiment of the two-sided etching process, the blade
29 array pattern of any of the embodiments of the present invention is etched
30 into the top surface 49 of sheet 6. A second pattern equivalent to the area

1 bounded by each of the openings 8 (e.g., rectangular) is etched into the
2 bottom surface 48 such that each of the blades in the blade array pattern is
3 thinner than the surrounding sheet 6. As a result, the sheet 6 forms a strong
4 base and as the punch 54 deforms the blades 4 downward, each of the
5 blades plastically deforms so as to produce blades that are straighter and
6 more truly perpendicular to the sheet.

7 In one embodiment of the etching process, a dry resist (e.g.,
8 "Dynachem FL" available from Dynachem located in Tustin, CA) is applied
9 12.5 μm thick to one or both sides of the sheet and exposed in a standard
10 manner. Then a suitable spray etcher (e.g., "Dynamil VRP 1 0/NM" available
11 from Western Tech. Assoc. located in Anaheim, CA) is used to spray) a
12 mixture of ferric chloride and hydrochloric acid onto the resist and sheet at
13 52°C (125 °F for two minutes. A standard caustic stripper is used for the
14 resist removal.

15 In another embodiment of the etching process, a wet resist (e.g.,
16 "Shipley 111S" available from Shipley Corporation, located in Marlborough,
17 MA) is applied 7.5 μm thick at about 20°C (70 °F) to one or both sides of the
18 sheet and exposed in a standard manner. Then a suitable etchant (e.g.,
19 ferric chloride) is sprayed onto the resist and sheet at 49°C (120 °F). A
20 standard caustic stripper is used for the resist removal.

21 Generally, the blades 4 are at an angle of about 90° to the surface 48
22 of the sheet 6 after being punched, but they can be disposed at any angle
23 forward or backward from the perpendicular position that will facilitate
24 penetration of and attachment to the stratum corneum. In one embodiment
25 (Figure 9), the blades are all aligned at an angle between about 1° and about
26 89° degrees, preferably about 10° to about 60°, more preferably about 20° to
27 45° to facilitate the device being slid along and into the skin. The angled
28 blades have two principal advantages. First, penetration of the blades is not
29 opposed by the elasticity of the skin because the blades are slid horizontally
30 into the skin as opposed to pressing vertically on the skin. Second, the

1 angled blades act to anchor the device in the skin as any motion of the skin is
2 less likely to dislodge the blades. In addition, other anchoring elements such
3 as barbs, openings, etc. can be used with the angled blades to further
4 enhance anchoring of the device.

5 In one embodiment (Figure 29), anchoring of the device is achieved by
6 coating the surface 48 of sheet 6 and surface 82 of each blade 4 with an
7 adhesive. One method of producing this embodiment comprises spraying the
8 adhesive on the device 2 along the direction indicated by arrows 84. In this
9 embodiment, the agent is free to pass through the openings 8 and along
10 surface 86 of each blade unencumbered by the adhesive. It is also possible
11 to apply the adhesive on only surface 48 and not on the blade surfaces 82.
12 This can be accomplished, for example, by applying the adhesive onto
13 surface 48 after the blades 82 have been punched by spraying the adhesive
14 in a direction which is parallel to the axis of the blades 82. It is further
15 possible to apply the adhesive only on the blade surfaces 82 and not on the
16 surface 48 of sheet 6 in order to anchor the device, although this last design
17 is the least preferred adhesive anchoring means.

18 The sheet and blades can be made from materials that have sufficient
19 strength and manufacturability to produce blades, such as, glasses,
20 ceramics, rigid polymers, metals and metal alloys. Examples of metals and
21 metal alloys include but are not limited to stainless steel, iron, steel, tin, zinc,
22 copper, platinum, aluminum, germanium, nickel, zirconium, titanium and
23 titanium alloys consisting of nickel, molybdenum and chromium, metals plated
24 with nickel, gold, rhodium, iridium, titanium, platinum, and the like. An
25 example of glasses include a devitrified glass such as "Photoceram" available
26 from Corning in Corning, NY. Examples of rigid polymers include but are not
27 limited to polystyrene, polymethylmethacrylate, polypropylene, polyethylene,
28 "Bakelite", cellulose acetate, ethylcellulose, styrene/acrylonitrile copolymers,
29 styrenetbutadiene copolymers, acrylonitrile/butadiene/styrene (ABS)

1 copolymers, polyvinyl chloride and acrylic acid polymers including
2 polyacrylates and polymethacrylates.

3 Very dense patterns can be created with unit cells wherein a unit cell
4 has a width A and a length B as illustrated in Figure 3. In one embodiment
5 (not shown), the pattern has the following characteristics: a unit cell area of
6 0.63 mm by 3.8 mm; the lineal length of a cut in a unit cell is approximately
7 equal to 15 mm; and the open skin length per square centimeter is 625 mm.

8 The microblades of the present invention make an elongated, thin
9 microcut (i.e., a slit) in the skin surface because the blades have a small
10 thickness (relative to their width and length) resulting in a minimal blade
11 cross-sectional area for the portions of the blade in the skin. The geometry of
12 the microblades 4 results in minimal blade volume in the skin with maximal
13 blade surface area in the skin. The advantages of the present invention
14 include, but are not limited to: (1) the thin blade geometry produces the
15 maximum drug percolation area for a given cross-section of the blade; (2)
16 minimal tissue damage occurs because the amount of blade material in the
17 skin and hence the volume loading is minimized; (3) slanted leading edges
18 (or equivalent pointed shapes) further minimize the amount of volume loading
19 or tissue damage while preserving a large percolation area; (4) for a given
20 volume loading, the larger the surface area, the larger the frictional retaining
21 force in the skin; and (5) for a given desired percolation area, there are fewer
22 blades necessary and therefore the force on each tip is higher making skin
23 penetration easier.

24 In other embodiments (Figures 10-16) other anchoring elements are
25 used in the present invention. In the embodiments shown in Figures 10-14,
26 prong 68 is etched in the side of some or all of the blades 4, and punched
27 lightly so as to protrude outward from the plane of each of the blades, as
28 illustrated in Figures 10 and 14. After the punching of the prongs, the blades
29 may be repunched to regain their substantially vertical orientation. Hinges 72
30 (Figure 13) can be used to control the retention force of the barb for

1 anchoring. The hinges allow for the retention force to be tailored
2 independently of the size of the blade because the force required to bend or
3 punch the prong is set independently of the size of the blades by the shape
4 or size of the hinge. In other words, the force can be tailored by the amount of
5 attachment of the prong to the plate, the greater the attachment, the greater
6 the force.

7 Prongs may protrude from either side of the blade, or both sides, if
8 desired. The shape of each prong can be any of a variety of shapes such as
9 triangular, square, etc. as shown in Figures 11 and 12. In another
10 embodiment, a curved protrusion 70 (Figures 15 and 16) is made by etching
11 a slit in some or all of the blades followed by punching. The prongs and
12 curved protrusions act to anchor the device in the skin similar to the manner
13 described previously.

14 In other embodiments other anchoring elements are used. In the
15 embodiments of Figures 17-19, the blade 4 has additional openings 74
16 extending through the blade to enhance anchoring. The edges forming the
17 holes or other linear openings are etched through the blade. Alternatively, or
18 in addition, numerous small pits (i.e., indentations) rather than holes can be
19 etched in the surface of the blade. As described above, the elastic nature of
20 the skin tissue causes the skin to move into the openings or pits. In the
21 embodiments with openings, the skin tissue may heal and reconnect through
22 the openings to provide even greater anchoring.

23 In a further embodiment (Figure 20), a plurality of blades in an opening
24 8 are arranged at 90° to another plurality of blades in an opening 8' such that
25 anchoring in two directions is obtained. In other words, the blades (not
26 shown) associated with the openings 8 are oriented parallel to the edge 76 of
27 the device 2 and the blades (not shown) associated with the openings 8' are
28 oriented parallel to the edge 78 of the device. The blades associated with
29 each opening 8 can be oriented at any angle with respect to the blades
30 associated with each opening 8'. Alternatively, the blades within each

1 opening can be along perpendicular sides of the openings. In a similar
2 manner, the blades within each opening can be formed in a serrated pattern
3 as illustrated in Figure 21. This pattern allows the blades to have different,
4 controllable angles with respect to each other defined by the angle of the
5 punch used and the etched angle β of the pattern.

6 The number of blades and openings of any of the embodiments of the
7 device 2 is variable with respect to the desired flux rate, agent being sampled
8 or delivered, delivery or sampling device used (i.e., electrotransport, passive,
9 ,osmotic, pressure-driven, etc.), and other factors as will be evident to one of
10 ordinary skill in the art. In general, the larger the number of blades per unit
11 area (i.e., the blade density), the more distributed is the flux of the agent
12 through the skin because there are a greater number of agent-conveying
13 pathways through the skin. Consequently, the smaller the number of blades
14 per unit area, the more concentrated is the flux of the agent through the skin
15 because there are fewer pathways. The present invention has a blade
16 density of at least about 10 blades/cm² and less than about 1000 blades/cm²,
17 preferably at least about 600 blades/cm², more preferably at least about 800
18 blades/cm². In similar fashion, the number of openings per unit area through
19 which the agent passes is at least about 10 openings/cm² and less than
20 about 1000 openings/cm². In one embodiment, the present invention
21 produces a percolation area of about 0.005 to .05 cm²/cm² of body surface,
22 preferably about 0.01 cm²/cm² of body surface.

23 One embodiment of the present invention relies on the application of
24 an electric current across the body surface or "electrotransport".
25 Electrotransport refers generally to the passage of a beneficial agent, e.g., a
26 drug or drug precursor, through a body surface such as skin, mucous
27 membranes, nails, and the like. The transport of the agent is induced or
28 enhanced by the application of an electrical potential, which results in the
29 application of electric current, which delivers or enhances delivery of the
30 agent or, for "reverse" electrotransport, samples or enhances sampling of the

1 agent. The electrotransport of the agents into or out of the human body may
2 be attained in various manners. One widely used electrotransport process,
3 iontophoresis, involves the electrically induced transport of charged ions.
4 Electroosmosis, another type of electrotransport process involved in the
5 transdermal transport of uncharged or neutrally charged molecules (e.g.,
6 transdermal sampling of glucose), involves the movement of a solvent with
7 the agent through a membrane under the influence of an electric field.
8 Electroporation, still another type of electrotransport, involves the passage of
9 an agent through pores formed by applying an electrical pulse, a high voltage
10 pulse, to a membrane. In many instances, more than one of these processes
11 may be occurring simultaneously to different extents. Accordingly, the term
12 "electrotransport" is given herein its broadest possible interpretation, to
13 include the electrically induced or enhanced transport of at least one charged
14 or uncharged agent, or mixtures thereof, regardless of the specific
15 mechanism(s) by which the agent is actually being transported.

16 It will be appreciated by those working in the field that the present
17 invention can be used in conjunction with a wide variety of electrotransport
18 drug delivery systems, as the invention is not limited in any way in this
19 regard. For examples of electrotransport drug delivery systems, reference
20 may be had to U.S. Patent Nos. 5,147,296 to Theeuwes et al., 5,080,646 to
21 Theeuwes et al., 5,169,382 to Theeuwes et al., and 5,169,383 to Gyory et al.,
22 the disclosures of which are incorporated by reference herein in their entirety.

23 Electrotransport devices generally use at least two electrodes which
24 are in electrical contact with some portion of the skin, nails, mucous
25 membranes, or other body surface. In the case of transdermal agent
26 delivery, one of the two electrodes is commonly referred to as the "donor" or
27 "active" electrode, and is the one from which the agent is delivered into the
28 body. In the case of transdermal agent sampling, one of the two electrodes is
29 referred to as the "receptor" electrode, and is the one into which the agent
30 (e.g., body electrolyte) is collected upon being withdrawn from the body. The

1 second electrode is typically termed the "counter" or "return" electrode, and
2 serves to close the electrical circuit through the body. For example, when the
3 agent to be delivered is a cation, i.e., a positively charged ion, the anode
4 becomes the active or donor electrode, while the cathode serves to complete
5 the circuit. Alternatively, if the agent to be delivered is an anion, i.e., a
6 negatively charged ion, the cathode is the donor electrode. When the agent
7 to be sampled is a cation, the cathode becomes the receptor electrode while
8 the anode serves to complete the circuit. When the agent to be sampled is
9 an anion, the anode becomes the receptor electrode while the cathode
10 serves to complete the circuit. When the agent to be sampled has no net
11 charge (e.g., glucose), then either the anode, or the cathode, or both
12 electrodes, can serve as the receptor electrode. Both the anode and cathode
13 may be donor electrodes if both anionic and cationic agents are delivered
14 simultaneously. Electrotransport delivery systems generally require at least
15 one reservoir or source of the agent to be delivered to the body.
16 Electrotransport sampling systems likewise require at least one reservoir in
17 which to collect the agent being sampled. Examples of such reservoirs
18 include a pouch or cavity as described in U.S. Patent No. 4,250,878 to
19 Jacobsen, a porous sponge or pad as described in U.S. Patent No. 4,141,359
20 to Jacobsen et al., and a pre-formed gel body as described in U.S. Patent No.
21 4,383,529 to Webster, among others. The pertinent portions of which are
22 incorporated herein by reference. Such reservoirs are electrically connected
23 to, and positioned between, the anode or the cathode and the body surface,
24 e.g., to provide a fixed or renewable source of one or more drugs in the case
25 of agent delivery. In addition, electrotransport systems also typically have an
26 electrical power source, e.g., one or more batteries, and an electrical
27 controller designed to regulate the timing, amplitude and/or frequency of the
28 applied electric current, and hence regulate the timing and rate of agent
29 delivery/sampling. This power source component is electrically connected to
30 the two electrodes. Optional electrotransport device components include a

1 counter reservoir, adhesive coatings, insulating separation layers, and
2 rate-controlling membranes.

3 Figures 1 and 22-25 illustrate a representative electrotransport
4 delivery/sampling device 10 that may be used in conjunction with the present
5 invention. Device 10 comprises an upper housing 16, a circuit board
6 assembly 18, a lower housing 20, anode electrode 22, cathode electrode 24,
7 anode reservoir 26, cathode reservoir 28 and skin-compatible adhesive 30.
8 Upper housing 16 has lateral wings 15 which assist in holding device 10 on a
9 patient's skin. Printed circuit board assembly 18 comprises an integrated
10 circuit 19 coupled to discrete components 40 and battery 32. Circuit board
11 assembly 18 is attached to housing 16 by posts (not shown in Figure 1)
12 passing through openings 13a and 13b, the ends of the posts being
13 heated/melted in order to heat stake the circuit board assembly 18 to the
14 housing 16. Lower housing 20 is attached to the upper housing 16 by means
15 of adhesive layer 30, the upper surface 34 of adhesive layer 30 being
16 adhered to both lower housing 20 and upper housing 16 including the bottom
17 surfaces of wings 15. Shown (partially) on the underside of circuit board
18 assembly 18 is a button cell battery 32. Other types of batteries may also be
19 employed to power device 10 depending on the need.

20 The device 10 is generally comprised of battery 32, electronic circuitry
21 19,40, electrodes 22,24, drug/receptor reservoir 26, counter reservoir 28, and
22 device 2, all of which are integrated into a self-contained unit. The outputs
23 (not shown in Figure 1) of the circuit board assembly 18 make electrical
24 contact with the electrodes 24 and 22 through openings 23,23' in the
25 depressions 25,25' formed in lower housing 20, by means of electrically
26 conductive adhesive strips 42,42'. Electrodes 22 and 24, in turn, are in direct
27 mechanical and electrical contact with the top sides 44',44 of drug reservoirs
28 26 and 28. The bottom side 46 of drug reservoir 28 contacts the patient's
29 skin through the opening 29 in adhesive layer 30. The bottom side 46' of
30 drug reservoir 26 contacts the patient's skin through the plurality of openings

1 8 in the device 2. The formulation of reservoir 26 is preferably a viscous gel
2 that fills the openings 8 such that the reservoir 26 is in direct contact with the
3 skin when the blades have penetrated the stratum corneum. The contact
4 between the reservoir and skin provides a path for the agent to be
5 transported along. If the reservoir 26 is not in direct contact with the skin
6 initially, typically sweat accumulates in the confined area and provides an
7 agent-transmitting pathway between reservoir 26 and the skin.

8 Device 10 optionally has a feature which allows the patient to
9 self-administer a dose of drug, or self-sample a body electrolyte, by
10 electrotransport. Upon depression of push button switch 12, the electronic
11 circuitry on circuit board assembly 18 delivers a predetermined DC current to
12 the electrode/reservoirs 22,26 and 24,28 for an interval of predetermined
13 length. The push button switch 12 is conveniently located on the top side of
14 device 10 and is easily actuated through clothing. A double press of the push
15 button switch 12 within a short time period, e.g., three seconds, is preferably
16 used to activate the device, thereby minimizing the likelihood of inadvertent
17 actuation of the device 10. Preferably, the device transmits to the user a
18 visual and/or audible confirmation of the onset of operation by means of LED
19 14 becoming lit and/or an audible sound signal from, e.g., a "beeper". Agent
20 is delivered/sampled through the patient's skin, e.g., on the arm, by
21 electrotransport over the predetermined interval. Anodic electrode 22 is
22 preferably comprised of silver and cathodic electrode 24 is preferably
23 comprised of silver chloride. Both reservoirs 26 and 28 are preferably
24 comprised of polymeric gel materials. Electrodes 22,24 and reservoirs 26,28
25 are retained by lower housing 20.

26 In the case of therapeutic agent (i.e., drug) delivery, a liquid drug
27 solution or suspension is contained in at least one of the reservoirs 26 and
28 28. Drug concentrations in the range of approximately 1×10^{-4} M to 1.0 M or
29 more can be used, with drug concentrations in the lower portion of the range
30 being preferred.

1 The push button switch 12, the electronic circuitry on circuit board
2 assembly 18 and the battery 32 are adhesively "sealed" between upper
3 housing 16 and lower housing 20. Upper housing 16 is preferably composed
4 of rubber or other elastomeric material, e.g., injection moldable ethylene vinyl
5 acetate. Lower housing 20 is preferably composed of a plastic or elastomeric
6 sheet material (e.g., polyethylene) which can be easily molded to form
7 depressions 25,25' and cut to form openings 23,23'. The assembled device
8 10 is preferably water resistant (i.e., splash proof) and is most preferably
9 waterproof. The system has a low profile that easily conforms to the body,
10 thereby allowing freedom of movement at, and around, the wearing site. The
11 reservoirs 26 and 28 are located on the skin-contacting side of the device 10
12 and are sufficiently separated to prevent accidental electrical shorting during
13 normal handling and use.

14 The device 10 adheres to the patient's body surface (e.g., skin) by
15 means of an adhesive layer 30 (which has upper adhesive side 34 and body-
16 contacting adhesive side 36) and the anchoring elements on the device 2 of
17 any of the embodiments discussed above. The adhesive side 36 covers the
18 entire underneath side of the device 10 except where the device 2 and
19 reservoir 28 are located. The adhesive side 36 has adhesive properties
20 which assures that the device 10 remains in place on the body during normal
21 user activity, and yet permits reasonable removal after the predetermined
22 (e.g., 24-hour) wear period. Upper adhesive side 34 adheres to lower
23 housing 20 and retains the electrodes and reservoirs within housing
24 depression 25,25' as well as retains device 2 to lower housing 20 and lower
25 housing 20 to upper housing 16.

26 In one embodiment of the drug delivery or sampling device there is a
27 bandage cover (not shown) on the device 10 for maintaining the integrity of
28 the device when it is not in use. In use, the bandage cover is stripped from
29 the device before the device is applied to the skin.

1 In other embodiments of the present invention, passive transdermal
2 delivery or sampling devices are used with device 2. Two examples of
3 passive transdermal delivery or sampling devices are illustrated in Figures 26
4 and 27. In Figure 26, passive transdermal delivery device 88 comprises a
5 reservoir 90 containing agent. Reservoir 90 is preferably in the form of a
6 matrix containing the agent dispersed therein. Reservoir 90 is sandwiched
7 between a backing layer 92, which is preferably impermeable to the agent,
8 and a rate-controlling membrane 94. In Figure 26, the reservoir 90 is formed
9 of a material, such as a rubbery polymer, that is sufficiently viscous to
10 maintain its shape. If a lower viscosity material is used for reservoir 90, such
11 as an aqueous gel, backing layer 92 and rate-controlling membrane 94 would
12 be sealed together about their periphery to prevent leakage. In a sampling
13 configuration, the reservoir 90 would initially not contain the agent. Located
14 below membrane 94 is microblade array device 2. The device 88 adheres to
15 a body surface by means of contact adhesive layer 96 around the periphery
16 of the device 2 and by the anchoring elements of any of the embodiments
17 described previously. The adhesive layer 96 may optionally contain agent. A
18 strippable release liner (not shown) is normally provided along the exposed
19 surface of adhesive layer 96 and is removed prior to application of device 10
20 to the body surface.

21 Alternatively, as shown in Figure 27, transdermal therapeutic device
22 98 may be attached to a body surface by means of a flexible adhesive
23 overlay 100 and the anchoring elements used in device 2. Device 98 is
24 comprised of an agent-containing reservoir 90 (for a delivery configuration)
25 which is preferably in the form of a matrix containing the agent dispersed
26 therein. In a sampling configuration, the reservoir 90 would initially not
27 contain the agent. An impermeable backing layer 102 is provided adjacent
28 one surface of reservoir 90. Adhesive overlay 100 maintains the device 98
29 on the body surface in combination with the anchoring elements of any of the
30 embodiments previously described for device 2. Adhesive overlay 100 can

1 be fabricated together with, or provided separately from, the remaining
2 elements of the device 98. With certain formulations, the adhesive overlay
3 100 may be preferable to the contact adhesive 96 shown in Figure 26. This
4 is true, for example, where the agent reservoir contains a material (such as,
5 for example, an oily surfactant permeation enhancer) which adversely affects
6 the adhesive properties of the contact adhesive layer 96. Impermeable
7 backing layer 102 is preferably slightly larger than reservoir 90, and in this
8 manner prevents the agents in reservoir 90 from adversely interacting with
9 the adhesive in overlay 100. Optionally, a rate-controlling membrane (not
10 shown in Figure 27) similar to membrane 94 in device 88 (Figure 26) can be
11 provided on the skin/mucosa side of reservoir 90. A strippable release liner
12 (not shown) is also normally provided with device 98 and is removed just prior
13 to application of device 98 to the body surface.

14 The formulation for the passive transdermal devices may be aqueous
15 or non-aqueous based. The formulation is designed to deliver the drug at the
16 necessary fluxes. Aqueous formulations typically comprise water and about 1
17 to 2 weight percent of a hydrophilic polymer as a gelling agent, such as
18 hydroxyethylcellulose or hydroxypropylcellulose. Typical non-aqueous gels
19 are comprised of silicone fluid or mineral oil. Mineral oil-based gels also
20 typically contain 1 to 2 weight percent of a gelling agent such as colloidal
21 silicon dioxide.

22 The reservoir matrix should be compatible with the delivered agent,
23 any excipients (e.g., flux enhancers, irritation preventing agents) and/or any
24 carrier therefore. When using an aqueous-based system, the reservoir matrix
25 is preferably a hydrophilic polymer, e.g., a hydrogel. When using a
26 non-aqueous-based system, the reservoir matrix is preferably composed of a
27 hydrophobic polymer. Suitable polymeric matrices are well known in the
28 transdermal drug delivery art.

29 When a constant drug delivery rate is desired, the drug is present in
30 the matrix or carrier at a concentration in excess of saturation, the amount of

1 excess being a function of the desired length of the drug delivery period of
2 the system. The drug may, however, be present at a level below saturation
3 without departing from this invention.

4 In addition to the drug, the matrix or carrier may also contain dyes,
5 pigments, inert fillers, permeation enhancers, excipients and other
6 conventional components of pharmaceutical products or transdermal devices
7 known in the art.

8 The amount of drug present in the reservoir and the size of the
9 reservoir is generally non-limited and is an amount equal to or larger than the
10 amount of drug that, in its released form, is effective in bringing about the
11 drugs physiological or pharmacological local or systemic effects.

12 The preferred form in which an agent is delivered or sampled generally
13 determines the type of delivery or sampling system to be used, and vice
14 versa. That is, the selection of a "passive" system which delivers or samples
15 the agent by diffusion or an electrically powered system which delivers or
16 samples the agent by electrotransport will be mostly determined by the form
17 of the agent. For example, with passive delivery systems, it has generally
18 been recognized that the agent is preferably delivered in either its free base
19 or acid form, rather than in the form of a water soluble salt. On the other
20 hand, with electrotransport delivery devices, it has been recognized that the
21 drugs should preferably be ionized and the drug salt should be soluble in
22 water. It is generally believed that the pathways for passive and
23 electrotransported transdermal drug delivery through intact skin are different,
24 with passive delivery occurring through lipid regions (i.e., hydrophobic
25 regions) of the skin and electrotransport delivery occurring through
26 hydrophilic pathways or pores such as those associated with hair follicles and
27 sweat glands. For the case of pierced skin, there is substantial passive flux
28 through the microslits created by the microblades piercing the stratum
29 corneum. The drug for passive delivery is generally hydrophobic, e.g., free
30 base form, whereas the preferred form of a drug for electrotransport delivery

1 is hydrophilic, e.g., water soluble salt form. For osmotic and pressure driven
2 systems which deliver or sample drugs by connective flow carried by a
3 solvent, the drug preferably has sufficient solubility in the carrier solvent. It
4 will be appreciated by those working in the field that the present invention
5 can be used in conjunction with a wide variety of osmotic delivery or sampling
6 systems, as the invention is not limited to a particular device in this regard.
7 Osmotic devices are disclosed for example in U.S. Patent Nos. 4,340,048 to
8 Eckenhoff, 4,655,766 to Theeuwes et al., and 4,753,651 to Eckenhoff, the
9 disclosures of which are incorporated by reference herein in their entirety.

10 This invention has utility in connection with the delivery of drugs within
11 any of the broad class of drugs normally delivered through body surfaces and
12 membranes, including skin. In general, this includes drugs in all of the major
13 therapeutic areas including, but not limited to, anti-infectives such as
14 antibiotics and antiviral agents, analgesics including fentanyl, sufentanil,
15 buprenorphine and analgesic combinations, anesthetics, anorexics,
16 antiarthritics, antiasthmatic agents such as terbutaline, anticonvulsants,
17 antidepressants, antidiabetic agents, antidiarrheals, antihistamines, anti-
18 inflammatory agents, antimigraine preparations, antinotion sickness
19 preparations such as scopolamine and ondansetron, antinauseants,
20 antineoplastics, antiparkinsonism drugs, antipruritics, antipsychotics,
21 antipyretics, antispasmodics, including gastrointestinal and urinary
22 anticholinergics, sympathomimetics, xanthine derivatives, cardiovascular
23 preparations including calcium channel blockers such as nifedipine, beta-
24 blockers, beta-agonists such as dobutamine and ritodrine, antiarrhythmics,
25 antihypertensives such as atenolol, ACE inhibitors such as ranitidine,
26 diuretics, vasodilators, including general, coronary, peripheral and cerebral,
27 central nervous system stimulants, cough and cold preparations,
28 decongestants, diagnostics, hormones such as parathyroid hormone,
29 bisphosphoriates, hypnotics, immunosuppressives, muscle relaxants,
30 parasympatholytics, pasympathomimetics, prostaglandins, psychostimulants,

1 sedatives and tranquilizers. The invention is also useful in conjunction with
2 reducing or preventing sensitization occurring as a result of electrotransport
3 delivery of proteins, peptides and fragments thereof, whether naturally
4 occurring, chemically synthesized or recombinantly produced. The invention
5 may additionally be used in conjunction with the delivery of nucleotidic drugs,
6 including oligonucleotide drugs, polynucleotide drugs, and genes.

7 The present invention has particular utility in the delivery of peptides,
8 polypeptides, proteins, nucleotidic drugs, and other such species through
9 body surfaces such as skin. These substances typically have a molecular
10 weight of at least about 300 daltons, and more typically have a molecular
11 weight of at least about 300 to 40,000 daltons. Specific examples of peptides
12 and proteins in this size range include, without limitation, LHRH, LHRH
13 analogs such as goserelin, buserelin, gonadorelin, napharelin and leuprolide,
14 GHRH, GHRF, insulin, insultropin, calcitonin, octreotide, endorphin, TRH,
15 NT-36 (chemical name: N-[(s)-4-oxo-2-azetidiny]carbonyl]-L-histidyl-L--
16 prolinamide), lypressin, pituitary hormones (e.g., HGH, HMG, desmopressin
17 acetate, etc), follicle luteoids, α ANF, growth factors such as growth factor
18 releasing factor (GFRF), β MSH, GH, somatostatin, bradykinin, somatotropin,
19 platelet-derived growth factor, asparaginase, bleomycin sulfate,
20 chymopapain, cholecystokinin, chorionic gonadotropin, corticotropin (ACTH),
21 erythropoietin, epoprostenol (platelet aggregation inhibitor), glucagon, HCG,
22 hirulog, hyaluronidase, interferon, interleukins, menotropins (urofollitropin
23 (FSH) and LH), oxytocin, streptokinase, tissue plasminogen activator,
24 urokinase, vasopressin, desmopressin, ACTH analogs, ANP, ANP clearance
25 inhibitors, angiotensin II antagonists, antidiuretic hormone agonists,
26 bradykinin antagonists, ceredase, CSI's, calcitonin gene related peptide
27 (CGRP), enkephalins, FAB fragments, IgE peptide suppressors, IGF-1,
28 neurotrophic factors, colony stimulating factors, parathyroid hormone and
29 agonists, parathyroid hormone antagonists, prostaglandin antagonists,
30 pentigetide, protein C, protein S, renin inhibitors, thymosin alpha-1,

1 thrombolytics, TNF, vaccines, vasopressin antagonists analogs, alpha-1
2 antitrypsin (recombinant), and TGF-beta.

3 As mentioned above, the device 2 of the present invention can also be
4 used with known sampling devices including, but not limited to, reverse
5 iontophoresis, osmosis, passive diffusion, phonophoresis, and suction (i.e.,
6 negative pressure). Figure 28 illustrates an osmotic sampling device 104 in
7 combination with any of the embodiments described previously for device 2.
8 Osmotic sampling devices can be used to sample any of a variety of agents
9 (e.g., body analytes, licit and illicit drugs) through a body surface including,
10 but not limited to glucose, body electrolytes, alcohol, blood gases, and illicit
11 substances such as drugs of abuse. The osmotic sampling device 104 is
12 attached to a body surface by means of a flexible adhesive overlay 100 and
13 the anchoring elements of device 2. Device 104 is comprised of a salt layer
14 106 located between a semi-permeable or osmotic membrane 94 and an
15 optional agent sensing element 108. The optional agent sensing element
16 can be any of a variety of chemically reactive sensors and indicators, for
17 example the color indicating test strips associated with glucose testing. The
18 adhesive overlay 100 can have a cut-out or transparent window in the area of
19 the indicators so that the indicators can be readily viewed. In an alternate
20 embodiment, the agent sensing element can be located between the device 2
21 and the salt layer.

22 The following example is merely illustrative of the present invention
23 and should not be considered as limiting the scope of the invention in any
24 way, as this example and other equivalents thereof will become apparent to
25 those versed in the art and in light of the present disclosure, drawings, and
26 the accompanying claims.

27

Example

The effect of the present design was evaluated on the skin resistance of a hairless guinea pig. A microblade array of two square centimeters was applied to ECG electrodes of five square centimeters. The blade array and electrodes were then applied to the skin of the animal. Resistance measurements were taken two minutes after application of the electrode to the skin of the animal. A decrease in resistance was observed indicating that penetration of the blades into the skin had occurred.

The device was evaluated for its effect on electrotransport flux of a decapeptide in the hairless guinea pig. The following are specifications for the device: the device consisted of a sheet having a plurality of rectangular openings having six blades, three on each long side of a 860 μm by 250 μm rectangle resulting in a 0.22 mm^2 open area for each opening. Each set of three blades started at the opposite end of the rectangle as the opposing set of blades. All of the blades were about 200 μm long. All six blades had slanted leading edges and the blade at each end was barbed as well. The group of six blades were arranged in two slightly offset rows with ten groups in each row on the sheet. Each device was a two cm^2 piece of stainless steel 25 μm thick etched and punched with eight pairs of offset rows or 160 groups of six blades for a total of 960 blades. There were 40 void areas per cm^2 and 240 blades per cm^2 .

For the study, a one compartment electrotransport system was used. It consisted of a cathode compartment containing a Dulbelco's phosphate buffered saline imbibing gel and a donor anode compartment containing two millimoles of decapeptide buffered at pH 7.5, 10% cholestyramine chloride and 3% hydroxyethylcellulose. After loading the gels in the system, the release liner was removed from the adhesive foam bottom of the electrotransport system. The device was carefully applied over a 1.6 cm diameter hole containing the donor gel with the microblades facing away from

1 the gel. The electrotransport system was then placed on the skin of a lightly
2 anesthetized hairless guinea pig. The systems were applied to the backs of
3 the animals using gentle downward pressure while at the same time pushing
4 bottom side of the system with the thumb of the technician. (The thumb
5 trapped a roll of the animals' skin which allowed some upward pressure to be
6 applied directly to the bottom side of the skin in contact with the device
7 microblades). After two minutes the current and resistance measurements
8 were observed and recorded. The electrotransport system was wrapped with
9 Vetrap and the animals were returned to their cages for the duration of
10 electrotransport (5 and 24 hours). Decapeptide flux was evaluated by
11 measuring urinary excretion of this peptide. Only a modest effect of the
12 device on decapeptide flux was observed in the first five hours of transport.
13 Between five and twenty-four hours, the electrotransport flux of an ordinary
14 electrotransport device dropped very significantly probably due to collapse of
15 the pathways or possibly aggregation of the peptide in the pathways (the
16 decrease in flux between five and twenty-four hours was reproducible). Use
17 of the blade array device completely prevented this decrease in flux and
18 resulted in an overall ten-fold increase in decapeptide flux over a twenty-four
19 hour transport period.

20 While the invention has been described in conjunction with the
21 preferred specific embodiments thereof, it is to be understood that the
22 foregoing description as well as the example are intended to illustrate and not
23 limit the scope of the invention. Other aspects, advantages and modifications
24 within the scope of the invention will be apparent to those skilled in the art to
25 which the invention pertains.